



PHOTOVOLTAIC ELEMENT MODULE AND ITS PRODUCTION METHOD,  
AND NON-CONTACT TREATMENT METHOD

BACKGROUND OF THE INVENTION

5 Field of the Invention

The present invention relates to a photovoltaic element module and its production method, and a non-contact treatment method, and more specifically to a photovoltaic element module comprising a plurality of electrically connected photovoltaic elements and a method of producing this module.

Related Background Art

The problem of global warming caused by the greenhouse effect, that is, an increase in CO<sub>2</sub> becomes larger, and therefore there is a growing demand for the development of a clean energy source that does not discharge CO<sub>2</sub>. One of such energy sources is nuclear power generation. Nuclear power generation, however, has many problems to solve such as radioactive wastes, so a safer clean energy source is desired. Of the expected clean energy sources, solar cells (photovoltaic elements) are gathering much attention due to their cleanness, safety, and easy handling.

At present, the solar cells are roughly classified into a crystal type using single-crystal or polycrystal silicon, an amorphous type using amorphous silicon, and a compound semiconductor type. Of these solar cells,

the amorphous type is highly expected. That is, despite its conversion efficiency lower than that of the crystal type solar cell, the amorphous silicon solar cell has excellent characteristics that are absent from the crystal type solar cell. For example, it can operate in the form of a film because the area of the amorphous type solar cell can be easily increased and has a large photoabsorption coefficient.

One of the reasons for the delayed diffusion of solar cells despite the attention being paid to them is their high costs. Various methods have been examined to reduce the production costs of solar cells. The representative approaches include:

(1) Reduction of the production costs of a photoelectric conversion layer,

(2) Efficient utilization of an electric power generating region,

(3) Reduction of the number of connections and thus connection material costs and labor costs for the connections, and

(4) Reduction of the use amount of covering materials and the material costs.

Of these approaches, the present invention particularly relates to the above point (3). The solar cell connection step is complicated and requires high reliability, while it required for simplification for cost reduction, reduction of the number of parts, and a

mass-productive connection method by automatization and high speed treatment.

5 Figs. 11A and 11B are schematic views showing an example of a photovoltaic element which is disclosed in, for example, Japanese Patent Application Laid-Open No. 8-139349 and which has been investigated by the inventors. Fig. 11A is a plan view of the photovoltaic element as seen from its light-receiving surface side, and Fig. 11B is a sectional view of the photovoltaic element shown in Fig. 11A, which is taken along the line 11B-11B in Fig. 11A.

10 A photovoltaic element 600 shown in Fig. 11, is produced by sequentially stacking a lower electrode layer 603, a semiconductor layer 604, and an upper electrode layer 605 on a conductive substrate 602 of, for example, stainless steel.

15 The upper electrode layer 605 comprises a transparent conductive film such as of indium oxide or indium tin oxide (ITO) and operates as both a reflection-preventing means and a current-collecting means.

20 A part of the transparent conductive film is linearly removed at a portion as shown by 601 (an etching line) in Fig. 11A by using screen printing or other methods of applying etching paste containing  $\text{FeCl}_3$  or  $\text{AlCl}_3$  to the film and heating it. A part of the transparent electrode film is removed in order to

prevent a short circuit from occurring between the substrate 602 and the upper electrode layer 605 when the outer circumference of the photovoltaic element is cut.

5 In addition, a current-collecting electrode 606 is formed on the surface of the upper electrode layer 605 to efficiently collect generated power. The current-collecting electrode 606 is formed by adhering a metal wire coated with the thin layer of a conductive  
10 adhesive (for example, a copper wire coated with a carbon paste) to the upper electrode layer 605 in order to obtain electric power generated in the semiconductor layer without loss. The copper wire is used in order to reduce power loss, and may be replaced by another  
15 highly conductive material.

Furthermore, a conductive foil 607 is provided as a further current-collecting electrode in addition to the current-collecting electrode 606. An insulating member 608 is provided under the conductive foil 607 to  
20 ensure the insulation provided by the etching line portion, the performance of which cannot be guaranteed.

In the photovoltaic element 600, the metal foil 607 and the substrate 602 function, respectively, as terminals of a positive and a negative electrodes to  
25 provide electric power.

It is difficult, however, for this photovoltaic element to be directly used for electric power

generation. Since the single photovoltaic element normally generates excessively low power, a plurality of photovoltaic elements must be connected in series or parallel to provide a desired voltage and current.

5 Fig. 11C is a plan view showing an example of series-connected photovoltaic elements (in the case of two series). In this figure, the conductive foil 607 of one photovoltaic element is electrically connected in series to the substrate 602 of another adjacent  
10 photovoltaic element by using a connection member 611. Solder is used for the connection and the series connection is completed by carrying out cleaning with a solvent such as MEK (methylethylketone) after  
15 soldering.

The conventional method of connecting photovoltaic elements to each other, however, has the following problems.

(1) To fix the conductive foil to the metal  
20 substrate by using solder, a part of the substrate must be heated to melt and fix the solder. The heat, however, is transferred through the thermally conductive metal substrate, and the semiconductor layer may degraded over a wide area to degrade their specific characteristics. In addition, defects may occur in the  
25 semiconductor layer depending on the heating temperature or time, thereby reducing the yield.

(2) The heating for melting and fixing the solder

may degrade the conductive adhesive provided on the semiconductor element to reduce the adhesion strength and electric conductivity, thereby reducing reliability.

5           (3) Since the solder must be melted, at least about ten seconds are required to heat and cool it, thereby reducing mass-productivity.

10           (4) If an automatic machine is used for mass production, it is difficult to control the temperature so as to achieve uniform soldering and to control the tip of a soldering iron. Thus, automation is difficult.

15           (5) Even when the solvent such as MEK is used to wipe off the excess solder, fluxes adhering to the substrate cannot be easily removed to cause rust under high-temperature and high-humidity conditions. Consequently, the covering material of the solar cell may be peeled off.

20           (6) The use of the soldering iron for connections may produce solder residue to reduce the yield. For example, the solder residue may penetrate between the adjacent photovoltaic elements connected in series to cause a short circuit therebetween.

25           On the other hand, the non-contact treatment method utilizing radiation of laser light or halogen light or electromagnetic waves is widely used in the processing treatment for materials such as etching,

welding, or cutting or in thermal treatment for semiconductor materials. Such a method can more or less solve the problems of the connections using solder.

5 It is important for the non-contact treatment, however, to efficiently absorb light, heat, or electromagnetic waves. When, for example, a material such as gold, silver, copper, or aluminum is used which are frequently used for electrodes for electric parts, 10 in particular, photovoltaic elements, these materials have a high surface reflectance with respect to the laser light and therefore exhibit a lower efficiency of absorbing energy. Thus, the idea for improving the absorption efficiency of energy is required. Also, a 15 method of improving the absorption efficiency of energy is required that can increase the efficiency of energy absorption without the needs for additional steps and that enables stable and high speed treatment.

## 20 SUMMARY OF THE INVENTION

It is an object of the present invention to solve the above problems in order to provide a photovoltaic element connection method that is reliable and easy to automate.

25 It is another object of the present invention to provide a photovoltaic element connection method and a laser treatment method that enables stable and high

speed treatment and that utilizes an energy-absorbing medium, and after treatment, the medium does not remain on the treated surface.

The present invention solves the above problems at a time to achieve the above objects. The present invention provides a photovoltaic element module comprising at least two photovoltaic elements electrically connected to each other, wherein a medium capable of absorbing at least 10% or more of a light having a wavelength of 0.4  $\mu\text{m}$  to 2.0  $\mu\text{m}$  is provided on an electric connection portion of the photovoltaic element.

In addition, the present invention provides a method of producing a photovoltaic module, which comprises a step of electrically connecting at least two photovoltaic elements to each other, wherein the step is a step of providing on a part of a first photovoltaic element a medium capable of absorbing at least 10% or more of a light having a wavelength of 0.4  $\mu\text{m}$  to 2.0  $\mu\text{m}$  and then irradiating the medium with the laser beam of wavelength 0.4  $\mu\text{m}$  to 2.0  $\mu\text{m}$  to electrically connect the first and second photovoltaic elements to each other.

Furthermore, the present invention provides a method of producing a photovoltaic module, which comprises a step of electrically connecting at least two photovoltaic elements to each other, wherein each



of the photovoltaic element has at least a conductive substrate, a semiconductor layer, and a light-transmissive electrode, and wherein the step is a step of electrically connecting the conductive substrate of a first photovoltaic element and the light-transmissive electrode of a second photovoltaic element to each other by laser welding.

Moreover, the present invention provides a non-contact treatment method of carrying out treatment by using an energy supply means for applying energy, which comprises placing a non-adhering medium capable of absorbing the energy on a material to be treated and irradiating the non-adhering medium with the energy.

Moreover, the present invention provides a method of producing a photovoltaic module, which comprises a step of electrically connecting at least two photovoltaic elements to each other, wherein the step is a step of placing a non-adhering medium capable of absorbing the energy on a part of a first photovoltaic element and irradiating the medium with energy to electrically connect the first photovoltaic element and a second photovoltaic element to each other.

#### BRIEF DESCRIPTION OF THE DRAWINGS

Figs. 1A and 1B are schematic views showing an appearance of a photovoltaic element module according to Example 1 of the present invention. Fig. 1A is a

plan view of the photovoltaic element as seen from its light-receiving surface side, and Fig. 1B is a sectional view of the photovoltaic element shown in Fig. 1A, which is taken along the line 1B-1B in Fig.

5 1A;

Fig. 2A is a plan view of two series-connected photovoltaic elements, each of which is shown in Figs. 1A and 1B, as seen from their light-receiving surface side. Fig. 2B is an enlarged view of the series-connected portion in Fig. 2A, and Fig. 2C is a sectional view of the portion as shown in Fig. 2B;

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Figs. 3A and 3B are schematic views showing an appearance of a photovoltaic element module according to Example 2 of the present invention. Fig. 3A is a plan view of the photovoltaic element as seen from its light-receiving surface side, and Fig. 3B is a sectional view of the photovoltaic element shown in Fig. 3A, which is taken along the line 3B-3B in Fig. 3A;

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Fig. 4A is a plan view of two series-connected photovoltaic elements, each of which is shown in Figs. 3A and 3B, as seen from their light-receiving surface side. Fig. 4B is an enlarged view of the series-connected portion in Fig. 4A, and Fig. 4C is a sectional view of the portion shown in Fig. 4B;

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Figs. 5A and 5B are schematic views showing an appearance of a photovoltaic element module according

to Example 3 of the present invention. Fig. 5A is a plan view of the photovoltaic element as seen from its light-receiving surface side, and Fig. 5B is a sectional view of the photovoltaic element shown in Fig. 5A, which is taken along the line 5B-5B in Fig. 5A;

Fig. 6A is a plan view of two series-connected photovoltaic elements, each of which is shown in Figs. 5A and 5B, as seen from their light-receiving surface side. Fig. 6B is an enlarged view of the series-connected portion in Fig. 6A, and Fig. 6C is a sectional view of the portion shown in Fig. 6B;

Figs. 7A and 7B are schematic views showing an appearance of a photovoltaic element module according to Example 4 of the present invention. Fig. 7A is a plan view of the photovoltaic element as seen from its light-receiving surface side, and Fig. 7B is a sectional view of the photovoltaic element shown in Fig. 7A, which is taken along the line 7B-7B in Fig. 7A;

Fig. 8A is a plan view of two series-connected photovoltaic elements, each of which is shown in Figs. 7A and 7B, as seen from their light-receiving surface side. Fig. 8B is an enlarged view of the series-connected portion in Fig. 8A, and Fig. 8C is a sectional view of the portion shown in Fig. 8B;

Figs. 9A and 9B are schematic views showing an

appearance of a photovoltaic element module according to Example 5 of the present invention. Fig. 9A is a plan view of the photovoltaic element as seen from its light-receiving surface side, and Fig. 9B is a sectional view of the photovoltaic element shown in Fig. 9A, which is taken along the line 9B-9B in Fig. 9A;

Fig. 10A is a plan view of two series-connected photovoltaic elements, each of which is shown in Figs. 9A and 9B, as seen from their light-receiving surface side. Fig. 10B is an enlarged view of the series-connected portion in Fig. 10A, and Fig. 10C is a sectional view of the portion shown in Fig. 10B;

Figs. 11A, 11B, and 11C are schematic views showing an appearance of a conventional photovoltaic element module. Fig. 11A is a plan view of the photovoltaic element as seen from its light-receiving surface side, Fig. 11B is a sectional view of the photovoltaic element shown in Fig. 11A, which is taken along the line 11B-11B in Fig. 11A, and Fig. 11C is a plan view of two series-connected photovoltaic elements as seen from their light-receiving surface side;

Fig. 12 is a sectional view schematically showing a configuration of the photovoltaic element;

Fig. 13 is a graph showing the reflective characteristics of metals;

Fig. 14 is a graph showing the relationship

between the photoabsorptivity of a medium and the welding stability;

Fig. 15 is a graph showing the welding stability of a light-absorbing medium;

5 Fig. 16 is a graph showing the relationship between the thickness of a film and the adhesive strength of the film after welding;

Fig. 17 is a schematic view showing a laser treatment method according to Example 6;

10 Figs. 18A and 18B are schematic views showing an appearance of a photovoltaic element module according to Example 7 of the present invention. Fig. 18A is a plan view of the photovoltaic element as seen from its light-receiving surface side, and Fig. 18B is a  
15 sectional view of the photovoltaic element shown in Fig. 18A, which is taken along the line 18B-18B in Fig. 18A;

Fig. 19A is a plan view of two series-connected photovoltaic elements, each of which is shown in Figs.  
20 18A and 18B, as seen from their light-receiving surface side. Fig. 19B is an enlarged view of the series-connected portion in Fig. 19A, and Fig. 19C is a sectional view of the portion shown in Fig. 19B;

25 Fig. 20 is a schematic view showing a method of supplying a non-contact medium;

Fig. 21 is a graph showing the relationship between the mean square surface roughness of the non-

contact medium and its welding reliability; and

Fig. 22 is a graph showing the relationship between the mean square surface roughness of the non-contact medium and its adhesion strength to a treated material.

#### DESCRIPTION OF THE PREFERRED EMBODIMENTS

Preferred embodiments of the present invention are described below with reference to the drawings.

(Photovoltaic element)

Fig. 12 schematically shows a sectional view of an example of a photovoltaic element used in the present invention. In this figure, numeral 701 indicates a substrate, 702 a lower electrode layer, 703 a semiconductor layer, and 704 an upper electrode layer. The photovoltaic element shown in Fig. 12 can be applied to an amorphous silicon type solar cell which desirably has flexibility. Such a configuration, however, can be applied to solar cells other than the amorphous type solar cells, such as a single-crystalline or polycrystalline solar cell or a solar cell using a semiconductor other than silicon or having the Schottky junction.

The substrate 701 is a member for mechanically supporting the semiconductor layer 703 in a thin solar cell of amorphous silicon type. The material for the substrate 701 may be conductive or insulating but must

be conductive when the substrate 701 also acts as an electrode. The substrate 701 must be durable enough to withstand the heating temperature for forming the semiconductor layer 703.

5           The conductive material for the substrate 701 includes metals such as Fe, Ni, Cr, Al, Mo, Au, Nb, Ta, V, Ti, Pt, and Pb; and alloys thereof, for example, a sheet metal such as brass or stainless steel; and composites thereof.

10           The electrically insulating material for the substrate 701 includes heat-resistant synthetic resins such as polyester, polyethylene, polycarbonate, cellulose acetate, polypropylene, polyvinyl chloride, polyvinylidene chloride, polystyrene, polyamide, 15 polyimide, and epoxy resin; and their composites with glass, carbon, boron, or metal fibers; glass; and ceramics.

(Lower electrode layer)

20           The lower electrode layer 702 is one of the electrodes for collecting electric power generated in the semiconductor layer 703 and must have a work function such that the lower electrode layer 702 forms an ohmic contact with a semiconductor.

25           The material for the lower electrode layer 702 includes metals such as Al, Ag, Pt, Au, Ni, Ti, Mo, Fe, V, Cr, Cu, stainless steel, brass, nichrome,  $\text{SnO}_2$ ,  $\text{In}_2\text{O}_3$ ,  $\text{ZnO}$ , and ITO (indium tin oxide); and alloys

thereof; and transparent conductive oxide (TCO).

The surface of the lower electrode layer 702 is desirably smooth, but may be textured when it irregularly reflects light. In addition, when the  
5 substrate 701 is conductive, the lower electrode layer 702 may be omitted.

The lower electrode layer 702 may be provided by a well-known method such as plating, deposition, or sputtering.

10 (Semiconductor layer)

The semiconductor layer 703 of the photovoltaic element used in the present invention comprises a well-known semiconductor material generally used for thin  
15 film solar cells. Specifically, it is possible to use as the semiconductor layer 703, a pin-junction amorphous silicon layer, a pn-junction polycrystalline silicon layer, or a layer of a compound semiconductor such as  $\text{CuInSe}_2/\text{CdS}$ .

When the semiconductor layer 703 is an amorphous  
20 silicon layer, it can be formed by introducing a raw material gas such as silane gas for forming a film, into a plasma CVD apparatus for generating plasma discharge. In addition, when the semiconductor layer 703 is a pn-junction polycrystalline silicon layer, it  
25 can be formed by forming a film using a molten silicon. When the semiconductor layer 703 consists of a compound semiconductor such as  $\text{CuInSe}_2/\text{CdS}$ , it can be formed by



the electron beam deposition method, the sputtering method, or the electrodepositon method.

(Upper electrode layer)

5 The upper electrode layer 704 is one of the electrodes for collecting electromotive force generated in the semiconductor layer 703 and is paired with the lower electrode layer 702. Like the lower electrode layer 702, the upper electrode layer 704 must have a work function such that the layer 704 forms an ohmic contact with a semiconductor. The upper electrode layer 704 is required when the semiconductor layer 703 comprises a semiconductor such as amorphous silicon having a high sheet resistance, and is not particularly required when a crystalline semiconductor is used, due to its low sheet resistance.

10 When the substrate 701 is opaque, the upper electrode layer 704 is necessarily located on the light incident side. In this case, the upper electrode layer 704 must transmit light, that is, must be a transparent electrode. To allow light from the sun or a while fluorescent lamp to be efficiently absorbed by the semiconductor layer 703, the light transmittance of the upper electrode layer 704 is preferably 85% or more.

20 In addition, to allow a photoelectric current generated in the semiconductor layer 703 to efficiently flow in a direction parallel with the semiconductor layer 703, the sheet resistance of the upper electrode layer 704

is preferably  $100\Omega/\square$  or less. The material having these characteristics and preferred for the upper electrode layer includes metal oxides such as  $\text{SnO}_2$ ,  $\text{In}_2\text{O}_3$ ,  $\text{ZnO}$ ,  $\text{CdO}$ ,  $\text{CdSnO}_4$ , and ITO ( $\text{In}_2\text{O}_3+\text{SnO}_2$ ).

- 5 (Non-contact treatment and method of producing photovoltaic element module)

The non-contact treatment according to the present invention can be applied to welding or cutting of various parts including electric parts or general  
10 structures formed of either a metal material or a non-metal material by energy irradiation, to etching or patterning during a step of producing an electric-part, and to the thermal treatment of semiconductor materials.

- 15 In the present invention, laser welding is applied to particularly photovoltaic elements. The energy supply means used in the present invention and the medium capable of absorbing energy are described below which are the features of the photovoltaic element  
20 module according to the present invention.

(Energy supply means)

- As the energy supply means according to the present invention, light, heat or electromagnetic waves can be suitably used. Heating by irradiation of light  
25 such as laser light or light from a halogen lamp or a far infrared lamp.

The laser used for laser welding according to the

present invention includes a solid laser such as ruby ( $\text{Cr}^{3+}$ :  $\text{Al}_2\text{O}_3$ ), YAG ( $\text{Nd}^{3+}$ :  $\text{Y}_3\text{Al}_5\text{O}_{12}$ ), phosphate glass, silicate glass, YLF ( $\text{Nd}^{3+}$ :  $\text{LiYF}_4$ ), or Thailand sapphire ( $\text{Ti}^{3+}$ :  $\text{Al}_2\text{O}_3$ ), and a gas laser such as  $\text{CO}_2$ -laser-excited or discharge-excited far infrared radiation or rare gas ions.

The metal material used for a system such as a solar cell through which a high current flows preferably has a low resistance in order to reduce losses caused by the resistance. As shown in Fig. 13, however, the reflectance is relatively high when the metal is irradiated with light having a wavelength of  $0.4 \mu\text{m}$  or more, it has been difficult that laser light having a wavelength of  $0.4 \mu\text{m}$  or more is used to weld the metal. On the other hand, the use of laser light of less than  $0.4 \mu\text{m}$  increases the costs of facilities as in excimer lasers. Accordingly, the use of laser light having a wavelength not more than  $0.4 \mu\text{m}$  has been limited to high-value-added products.

The present invention enables laser light having a wavelength of  $0.4 \mu\text{m}$  or more to be used to welder metal.

Of the lasers having a wavelength of  $0.4 \mu\text{m}$  or more, solid lasers (the wavelength of main solid lasers is in a range of  $0.4 \mu\text{m}$  to  $2.0 \mu\text{m}$ ) is more efficient than gas lasers and has advantages of providing a higher-power laser light and enabling the apparatus to

be compactified. In particular, YAG lasers have excellent characteristics such as their capabilities of transmitting laser light through optical fibers and executing welding at a position remote from a laser transmitter. They also enable the welding conditions to be changed by the selection of optical fibers and outgoing units and also enable one laser beam to be divided into about 2 to about 10 beams.

(Medium capable of absorbing energy)

The reflective characteristic obtained when metal is irradiated with light depends on the type of metal, and is as shown in Fig. 13. Despite the amount of reflection depending on the wavelength, most irradiation light is reflected particularly at the long wavelength side. For example, at  $0.7 \mu\text{m}$ , which is close to the wavelength of ruby laser beams ( $0.69 \mu\text{m}$ ), the reflectances of gold, silver, copper, and aluminum are 97.0%, 98.5%, 97.5%, and 89.8%, respectively. The reflectances at the YAG laser wavelength ( $1.06 \mu\text{m}$ ) of gold, silver, copper, and aluminum are 98.2%, 98.9%, 98.5%, and 93.9%, respectively. Thus, it has been difficult to weld metal such as gold, silver, copper, and aluminum used for photovoltaic elements, by using the ruby or YAG laser.

<Medium capable of absorbing at least 10% or more of laser light having wavelength of  $0.4 \mu\text{m}$  to  $2.0 \mu\text{m}$ >

Thus, in the present invention, a medium capable

of absorbing 10% or more of laser light is provided on a surface to be welded to reduce inappropriate welding while enabling stable laser welding. In particular, the medium preferably has an absorptivity of 10% or more at 0.4  $\mu\text{m}$  to 2.0  $\mu\text{m}$ , which is in the wavelength range of the above solid laser.

Fig. 14 shows the effects obtained by providing a medium capable of absorbing 10% or more of laser light on a surface to be welded.

Fig. 14 is a graph showing the relationship between the photoabsorptivity of the medium and welding stability obtained when a copper foil and a silver-plated copper foil (each having a thickness of 100 $\mu\text{m}$ ) having a high reflectance were selected as a metal to be irradiated with laser light and when a paint was applied uniformly to the surface of the metal as the medium, followed by the irradiation of YAG laser beams (wavelength: 1.06 $\mu\text{m}$ ) to carry out welding. A plurality of paints having different photoabsorptivities were used for evaluations. In addition, welding was carried out under conditions optimal for each reflectance (however, copper and silver-plated copper were welded under the same conditions). Furthermore, in evaluation of the welding stability, a sample after welding which exhibited a joining force of 4.0 kg or more after thermal cycle tests (200 cycles at 90°C to -40°C) and in which no holes or cracks were found in the welded

portion when observed using an optical microscope was regarded as a good product (non-defective product). Thus, all the obtained samples were evaluated based on the non-defective percentage.

5        Since copper and silver reflect 98.0% or more of laser light having a wavelength of 1.06  $\mu\text{m}$ , the welding stability of the metal is normally 40% or less, they are difficult to be subjected to laser welding. As shown in Fig. 14, however, by providing a medium  
10        capable of absorbing light on the surface of the metal, it is possible to improve the welding stability of the metal. In particular, the welding stability is 80% or more when the medium has a photoabsorptivity of 10% or more.

15        The energy (welding energy) required for welding a metal by using laser light can be represented by the following equation.

$$\text{(Welding energy)} = \text{(laser outgoing energy)} \times \text{(photoabsorptivity of metal)}$$

20        Normally, when a metal is welded using laser light, laser light having a larger energy than the welding energy must be supplied in consideration of the surface reflection of the metal. If, for example, the metal has a light reflectance of 90%, it is necessary  
25        to irradiate the metal with light having a laser outgoing energy which is 10 times as large as that required for metal welding in the case of no reflection

of a metal. Once laser light is introduced into the metal, the metal is melted and the molten metal readily absorbs laser light. Consequently, most supplied energy becomes welding energy. When, however, the metal is, for example, a thin foil used for a photovoltaic element, excessive energy may increase the temperature of the irradiated portion above the melting point of the metal, resulting in holes in the metal.

In the present invention, a medium capable of absorbing laser light having a wavelength of 0.4  $\mu\text{m}$  to 2.0  $\mu\text{m}$  is provided on the surface of a metal to be irradiated with laser light to restrain the reflection from the surface of the metal and allow laser light to be easily introduced into the metal. For example, in the case of executing welding that requires 5J energy, 50J outgoing energy is required when the reflectance of the metal is 90%, whereas it is possible to execute welding with 25J outgoing energy when the reflectance of the surface can be reduced to 80% by using a medium. That is, by providing a light-absorbing medium on the surface of metal having high surface reflection, the outgoing energy of laser light can be remarkably reduced. This configuration can prevent holes from being formed in the metal.

Although the above discussion uses paints as the medium capable of absorbing light, the medium according to the present invention is not limited to paints but

may be selected as appropriate whether they are insulating or conductive materials. The insulating material used for the medium according to the present invention, however, must be melted when heated during welding to maintain the conductivity between the metal members.

Specifically, the object of the present invention can be sufficiently achieved by coloring the surface of the metal member using felt pen or ink jet. The color is preferably other than white so as to provide a larger photoabsorption coefficient. To improve the welding stability, an ink application method that enables ink to be uniformly applied is preferably used. Various methods can be used, for example, the hardening of a silk-screen-printed ink by using a hot air drying furnace.

In addition, instead of using an ink, a film material such as a black PET (polyethylene-terephthalate) film (for example, trade name: Lumirror X30, produced by Toray Industries, Inc.; and trade name: Melinex 427, produced by ICI Japan Ltd.) may be stuck to the surface of the metal member, and the metal member may be welded together with the film by irradiating it with laser light from the film side. After welding, the film is preferably removed, but may not be removed depending on the material of the film. When the thickness of the film is in a range of 5  $\mu\text{m}$  to



30  $\mu$ m, welding is stabilized to allow the film to be removed easily after welding.

Furthermore, when a conductive material is used as the medium, a metal material of a large photo-absorption coefficient may be selectively used.

Specifically, an iron based material such as stainless steel, a material plated with Ni or solder, a material obtained by treating in a strong-acid solution to oxidize or etch the surface of a metal, a material coated with carbon black, or a material with conductive fine particles dispersed therein may be located on the surface of the metal member, which is then welded together with the conductive material. After welding, the conductive material is preferably removed, but may not be removed depending on the material.

The metal member may be plated with Ni or solder to use the Ni or solder as the medium capable of absorbing light.

Fig. 15 shows examples of welding stability, which were obtained when the above-mentioned media and YAG laser were used to carry out welding. The details of the media shown in Fig. 15 are as follows.

Felt pen:	Oily Magic Ink No. 500
	Manual application
	Photoabsorptivity: 10%

Silk screen printing:	Emerson & Cuming CT-5079-3A
	(produced by National Starch

& Chemical Company)  
Printer

Photoabsorptivity: 60%

5            Ink jet printer:        JP-K27 (produced by Hitachi  
   Manufacturing Company)

Dedicated printer

Photoabsorptivity: 25%

10            Black PET tape:            Melinex 427 (produced by ICI  
   Japan Ltd.)

(Lumilar X (produced by Toray Industries, Inc.) or  
black-treated Lumilar T (produced by Toray Industries,  
Inc.)

Photoabsorptivity: 60%

15            Ni plating:                    Thickness: 2  $\mu$ m to 5  $\mu$ m

Photoabsorptivity: 50%

Surface oxidation:        Electrolytic treatment

Photoabsorptivity: 20%

20            All the media provided satisfactory results, that  
is, their welding stabilities were 70% or more.

<Non-adhering medium>

The following materials are applicable as the non-  
adhering medium according to the present invention.

25            The applicable materials include paper; a cloth; a  
leather; a thin metal foils such as stainless steel,  
steel, and black alumite; polyester films such as a  
polyethyleneterephthalate film, a polybutylene-

terephthalate film, a polyethylenenaphthalate film, a polycyclohexylenedimethyleneterephthalate film, and a polyethylenebisphenoxycarboxylate film; polyolefin films such as polyethylene film and polypropylene; 5 cellulose derivative film such as a cellulose acetate butylate film and a cellulose acetate propionate film; vinyl resin films such as a polyvinyl chloride film and a polyvinylidene chloride film; polymer films such as polystyrene film, a polyamide film, a polyimide film, a 10 polycarbonate film, a polysulfone film, a polyurethane resin film, an epoxy resin film, and a fluoride resin; and a composite material comprising the above polymer film laminated with a thin metal foil such as a stainless steel foil, a steel foil, or a black alumite 15 foil.

When the medium has at least the polymer film among the above materials, the polymer film is thin and strong and can be removed easily after welding because the polymer film is melted and volatilized during energy 20 irradiation. In addition, the polymer films is supplied in a long size so that welding can be carried out with a high mass-productivity.

In addition, when the medium is a magnetic tape, the objects of the present invention are accomplished 25 most appropriately. This is because this material is excellent in workability, mold-releasing capability, and high-speed treatment. The mold-releasing

capability can be further improved by attaching the magnetic surface of the magnetic tape to a material to be treated.

Furthermore, the surface of the non-adhering medium which attaches to a material to be treated preferably has a surface roughness of 0.1 nm to 5,000 nm. In the case of the roughness of 5,000 nm or less, the non-adhering medium efficiently guides, for example, laser light to the material to be treated as shown in Fig. 21. When the surface of the non-adhering medium which is attached to the material to be treated has a surface roughness of 0.1 nm or more in mean square, the non-adhering medium is unlikely to stick to the treated material during laser treatment, for example, as shown in Fig. 22, thereby allowing the non-adhering medium to be easily removed after laser treatment.

The methods of providing on at least the side of the medium which contacts the material to be treated by energy irradiation, recessed and protruding portions corresponding to a surface roughness of 0.1 to 5,000 nm in mean square include the use of the characteristics of the material itself for the medium, the surface treatment by means of etching or discharge, the deformation of the surface shape by means of pressing or scratching, the mixing of a carbon block or a color material such as pigment into the polymer film, or the

application or deposition of a selected material.

As one example of using the polyethylene-  
terephthalate film, the protrusions on the surface of  
the polyethyleneterephthalate film can be controlled by  
5 the selection of a polymerization medium for a raw  
material polymer or by adding inorganic particles to  
the film, as disclosed in Japanese Patent Publication  
No. 30-5639. More specifically, there is a method of  
adding an oxide such as  $\text{SiO}_2$ ,  $\text{TiO}_2$ ,  $\text{CaCO}_3$ , or  $\text{Al}_2\text{O}_3$  or an  
10 inorganic salt during the polymerization of the raw  
material polymer or during the melting of pellets prior  
to drawing.

In addition, the material which is applied or  
deposited material onto the medium includes carbon  
15 black, graphite, titanium oxide, barium sulfate, zinc  
sulfide, magnesium carbonate, calcium carbonate, zinc  
oxide, calcium oxide, magnesium oxide, tungsten  
disulfide, molybdenum disulfide, boron nitride, tin  
disulfide, silicon disulfide, chromium oxide, alumina,  
20 silicon carbide, cerium oxide, corundum, artificial  
diamond, iron oxide, garnet, silica rock, silicon  
nitride, molybdenum carbide, boron carbide, tungsten  
carbide, titanium carbide, diatomaceous earth,  
dolomite, a lubricant such as resin powders, an  
25 abrasive, an anti-static agent, a dispersant, a  
pigment, and/or dyes which may be combined with the  
above materials, such as a phthalocyanine dye, an azo

dye, an anthraquinone dye, an indigoid dye, a nitro and nitroso dyes, a quinoline dye, a methyne dye, a thiazole dye, a quinoneimine dye, an azine dye, an oxazine dye, an thiazine dye, an azoic dye, a diphenylmethane dye, a triphenylmethane dye, a xanthene dye, acridine dye, an oxidation dye, a sulfidization dye, a phthalein dye, an aminoketone dye, or an oxyketone dye.

Paper, a cloth, or a material coated with a pigment such as carbon black by using a nozzle coater is preferably used as a non-adhering anti-reflection medium because "residue" resulting from heat during laser treatment is unlikely to stick to the treated material.

The means for supplying the non-adhering medium is not particularly limited and may handle a sheet medium or a roll medium. However, the medium can be preferably attached and detached to such means and desirably continuously supplied in consideration of mass production.

When a sheet-like medium is supplied, it may have to be replaced at the end of each treatment or a means may be required for offsetting a position so as to avoid irradiating the same position with energy. Thus, the medium is preferably supplied from the form of a roll and is desirably wound up after treatment. When the medium is shaped like a roll, it can be

continuously supplied by using a simple delivery and winding mechanisms, thereby enabling mass production. (Material to be treated)

The material to be treated may be selected from various metal materials or non-metal materials and is not limited. The present invention, however, is particularly effective for a material having a low absorption characteristic with respect to an used energy. Specifically, the present invention is effective for a high-reflection material having reflectance of 40% or more of an used energy, or transmittance of 40% or more of an used energy.

As the specific metal material to be treated, it is possible to use a metal such as Fe, Ni, Cr, Al, Mo, Au, Nb, Ta, V, Ti, Pt, Pb, Ag, or Cu, or an alloy thereof, for example, stainless steel, brass, or nichrome. In particular, as a metal material used for an electrode for an electric part through which a current flows, a material such as gold, silver, copper, or aluminum is preferably used that has a low resistance to reduce resistance losses. Laser light, however, is noticeably reflected from the above metals as described above (Fig. 13), it has been difficult to directly irradiate these metals with laser light having a wavelength of 0.4  $\mu\text{m}$  or more. Laser light having a wavelength less than 0.4  $\mu\text{m}$  require expensive facilities as in excimer lasers, and is unlikely to supply a high energy

required for welding or cutting. Consequently, the application of such laser light has been limited.

In addition, as the non-metal material to be treated, it is possible to use a synthetic resin such as polyester, polyethylene, polycarbonate, cellulose acetate, polypropylene, polyvinyl, chloride, polyvinylidene chloride, polystyrene, polyamide, polyimide, an epoxy resin, or a fluororesin; glass fibers, carbon fibers, or boron fibers, and glass or ceramics.

The material to be removed or the semiconductor material to be thermally treated by laser light during etching or patterning in the step of producing an electric part includes single-crystalline silicon, polycrystalline silicon, amorphous silicon, or compound silicon such as  $\text{CuInSe}_2/\text{CdS}$ , and  $\text{SnO}_2$ ,  $\text{In}_2\text{O}_3$ ,  $\text{ZnO}$ , or ITO (indium tin oxide).

The connection method according to the present invention has been accomplished by the inventors conducting experiments and detailed investigations in order to realize a method which is reliable and can be easily automated in production of a photovoltaic element module by electrically connecting at least two photovoltaic elements in series or in parallel. This method has the following effects.

(1) Since operations are completed for a time shorter than that in the conventional techniques and a



welding point has a smallest area, the present invention has few portions adversely affected by heat. Thus, it can obtain almost all the specific characteristics of the semiconductor. This effect can be further improved by separating a portion where welding is carried out by laser from effective areas via etching lines.

(2) In connecting photovoltaic elements each comprising a semiconductor element provided on the metal substrate, the metal substrate separated from the effective areas via etching lines can be directly used as an output terminal electrode, thereby omitting the step of forming a terminal to reduce the non-electric power-generation area. This also applies to conductive substrates other than metal substrates.

(3) In electrically connecting adjacent photovoltaic elements to each other, a metal member is provided on the electrode portion of the semiconductor element and the metal members of the photovoltaic elements were electrically connected to each other by using laser welding. Therefore, the semiconductor is not almost affected by the adverse effect of heat, thereby avoiding restrictions on the connection form to enable arbitrary designs.

(4) A conductive adhesive can be used to join the semiconductor layer and collecting electrode of the photovoltaic element together and to join together the

collecting electrode of the photovoltaic element and the metal member provided on the electrode portion in order to simplify the steps, In the conventional techniques using solder, heating for melting and fixing solder causes the conductive adhesive to be degraded to reduce the yield. The present invention, however, solves this problem to enable the conductive adhesive to be used in the steps of producing a photovoltaic element module.

(5) When the metal members are welded together by laser light, the metal material has a reflection characteristic such as that shown in Fig. 13, and therefore laser light is required to have a higher energy by the surface reflection losses of the metal than that actually required for welding. However, once laser light is introduced into the metal, the metal is melted and readily absorbs laser light, thereby changing most of the supplied energy to welding energy. In this case, when the metal member is, for example, a thin foil used for a thin photovoltaic element, an excessive amount of energy increases the temperature of the portion irradiated with laser light above the boiling point of the metal to cause holes to be formed in the metal member. In the present invention, a medium capable of absorbing 10% or more of laser light having a wavelength of 0.4  $\mu\text{m}$  to 2.0  $\mu\text{m}$  is provided on the surface of the metal member to restrain the

reflection from the surface of the metal member in order to allow laser light to be easily introduced into the metal member. This configuration can reduce the outgoing energy of the laser to simplify the welding of metal with high surface reflection, and stabilizes the welding strength, thereby providing a reliable photovoltaic element module. In addition, the outgoing energy can be restricted to increase the lifetime of an expensive outgoing lamp, thereby reducing running costs.

(6) An excellent solar cell can be provided by forming a metal member consisting of at least one of gold, silver, copper, stainless steel, and aluminum as a main component. The metal member from which electric power generated by the photovoltaic element is externally obtained is required to be a conductive material that minimizes output losses and have a high weather resistance, for example, a long-term stability. A very conductive photovoltaic element module having few resistance losses can be provided by using one of gold, silver, copper, stainless steel, and aluminum. In particular, stainless steel can be used to provide a relatively inexpensive photovoltaic element module that has a rust and a weather resistances.

(7) The method of providing on the surface of the metal member irradiated with laser light a medium capable of absorbing 10% or more of laser light having

a wavelength of 0.4  $\mu\text{m}$  to 2.0  $\mu\text{m}$  includes a method of using as a medium a part of the metal member used for the photovoltaic element, and a method of supplementarily supplying a medium during the production step, one of which can be selectively used. The method of using a part of the metal member as the medium includes a method of treating the metal member in a strong-acid solution to oxidize or etch its surface, a method of plating the surface of the metal member, and a method of coating the surface of the metal member with carbon black. In addition, the method of supplementarily supplying the medium during the production step includes a method of closely contacting a material of a low surface reflectance to the surface of the metal member and irradiating the metal member with laser light from the side of the material of a low surface reflectance to weld the metal member together with the material of a low surface reflectance. After welding, the material is preferably removed but may not be removed depending on the material.

(8) When the medium capable of absorbing light is a color ink provided on the surface of the metal member, it can be provided most simply. The method of providing the color ink includes a method of applying the ink by using a felt pen, a method of jetting the ink, and a method of printing the ink by using silk

screen printing, one of which can be selectively used. Even when metal is used that is easy to reflect laser light, a color ink can be provided on the surface of the metal to allow laser light to be easily introduced into the metal, thereby providing a stable welding strength to form a very reliable photovoltaic element module.

(9) The most stable welding strength can be obtained when the medium capable of absorbing laser light which is provided on the surface of the metal member is a film having a thickness of 5  $\mu\text{m}$  and 30  $\mu\text{m}$ . Based on the film characteristics, the film material is selected so as to match the wavelength of laser light used, and is advantageous in controlling quality such as thickness. In addition, when the metal member is irradiated with laser light from the film side to weld the metal member with the film, the film can be easily peeled off after welding when the thickness of the film is from 5  $\mu\text{m}$  to 30  $\mu\text{m}$ .

(10) When the medium capable of absorbing laser light which is provided on the surface of the metal member consists of at least Fe, Ni, or solder, the welding strength can be stabilized, and the number of operations can also be reduced by previously providing Fe, Ni, or solder on the surface of the metal member using plating. The material for the metal member from which electric power generated by the photovoltaic

element is externally obtained must be conductive to minimize output losses and must have a weather resistance such as long-term stability, and therefore a material plated with Fe, Ni, or solder is preferably  
5 used when the metal member comprises, for example, copper.

The non-contact treatment of the present invention is an improved non-contact treatment using, for example, laser or halogen light to cut or weld a high-  
10 reflection material such as gold, silver, copper, or aluminum that is often used for electric parts such as photovoltaic elements, and has been obtained by the inventors conducting experiments to obtaining knowledge and executing further investigations. In addition to  
15 the effects described in the above (1) to (6), this method has the following effects.

(11) The present invention provides a non-contact treatment method of carrying out treatment by supplying energy from an energy supply means, comprising placing  
20 on a material to be treated a non-adhering medium capable of absorbing energy and irradiating the non-adhering medium with energy. This method can achieve stable non-contact treatment because the physical characteristics of the placed medium determines the  
25 reflectance, and enables high-speed treatment because the non-adhering anti-reflection material can be removed after the non-contact treatment.

(12) When the surface of the non-adhering medium that closely contacts the material to be treated has a surface roughness of 0.1 nm to 5,000 nm in mean square, more stable welding is possible and the non-adhering anti-reflection material can be removed easily. Beyond 5,000 nm, stable treatment is impossible because the medium does not closely contact the material, whereby energy is not efficiently introduced to the inside of the material to be treated. In addition, below 0.1 nm, the non-adhering medium closely contacts the material to be treated but significantly sticks to the material during energy irradiation, whereby the medium is not easily removed after the treatment.

(13) When the non-adhering medium has at least a polymer film, that is, when it is, for example, a polyethyleneterephthalate film mixed with carbon black, a polyethylenenaphthalate film with carbon black coated or deposited on its surface, or a material with a stainless steel foil laminated thereon, it can be removed more easily after energy irradiation because the above material is very strong and thin and because the polymer film is dissolved and volatilized during energy irradiation. In addition, polymer films are supplied in a long size enough to easily enable mass production.

(14) The effect of the present invention can be most effectively exhibited when the non-adhering medium

is a magnetic tape. The magnetic tape is excellent in stable workability, mold-releasing capability, and high-speed treatment. The mold-releasing capability can be improved by closely contacting the surface of the magnetic tape with the material to be treated.

(15) An object of the present treatment method is to efficiently guide energy to the material to be treated, and the particularly suitable energy is light, heat, or electromagnetic waves.

(16) The anti-reflection material (non-adhering medium) is irradiated with energy while the non-adhering medium is holding the material to be treated, whereby the medium and the material closely contact each other stably to make treatment stable.

(17) Since the non-adhering medium is removed by energy irradiation and/or after non-contact treatment, no non-adhering medium remains in the treated part after the non-contact treatment, thereby preventing inconvenience in appearance and defects from occurring in post-process.

(18) When the non-adhering medium is supplied from the form of a roll of the medium and then is wound up after energy irradiation, it can be continuously supplied to enable mass production and to increase the treatment speed.

(19) An object of the present non-contact treatment is to achieve stable treatment, therefore it



is particularly suitable for welding or cutting.

(20) When the material to be treated is an electrode for an electric part, it can be joined stably and reliably. In particular, when the material to be treated is an electrode for a photovoltaic element, the non-adhering and anti-reflection medium does not remain on the electrode portion to improve the appearance while avoiding the need to account for the compatibility with a package material.

Examples of the present invention are described below.

(Example 1)

Figs. 1A to 2C are schematic views showing the appearance of a photovoltaic element module according to Example 1 of the present invention. Fig. 1A is a plan view of a photovoltaic element as seen from its light-receiving surface, and Fig. 1B is a sectional view of the photovoltaic element shown in Fig. 1A, which is taken along line 1B-1B in Fig. 1A. In addition, Fig. 2A is a plan view of two photovoltaic elements connected in series as seen from their light-receiving surface, Fig. 2B is an enlarged view of the series-connected portion in Fig. 2A, and Fig. 2C is a sectional view of Fig. 2B.

In Fig. 1A, reference numeral 100 indicates a 300 mm x 280 mm photovoltaic element comprising a substrate 102, a lower electrode layer 103, a semiconductor layer

104 consisting of amorphous silicon and having a photovoltaic function, and an upper electrode layer 105.

In this example, the substrate 102 for supporting the entire photovoltaic element comprises a stainless steel plate having a thickness of 150 $\mu$ m. An Al layer of about 2,000 Å in thickness and a ZnO layer of about 13,000 Å in thickness were sequentially formed on the substrate 102 as the lower electrode layer 103 by using the sputtering method. In addition, the semiconductor layer 104 was formed by sequentially stacking an n-, i-, p-, n-, i-, and p-type semiconductor layers this order from the substrate side by using the plasma CVD method. The thickness of these layers was about 150 Å, 4,000 Å, 100 Å, 100 Å, 800 Å, and 100 Å, respectively. In addition, the upper electrode layer 105 was a transparent electrode consisting of a thin indium oxide film of about 700 Å thickness, and was formed by depositing In in an O<sub>2</sub> atmosphere using the resistance heating method. Furthermore, to prevent an effective light-receiving area from being affected by the adverse effect of a short circuit between the substrate and the transparent electrode that may occur when the outer circumference of the photovoltaic element is cut, etching paste containing FeCl<sub>3</sub>, or AlCl<sub>3</sub> was coated on a part of the upper electrode layer 105 by using screen printing, and was heated and washed to linearly remove

the part of the upper electrode layer 105 in order to form an etching line 101.

Subsequently, a copper foil strip of 10 mm in width, 285 mm in length, and 100  $\mu$ m in thickness was formed near one side (280 mm long) of the back surface (on the substrate 102 side) of the photovoltaic element as a rear-surface-side conductive foil 109, using the method described in Japanese Patent Application Laid-Open No. 8-139349. One side of the copper foil strip protruded out from the photovoltaic element 100, as shown in Fig. 1A.

Subsequently, an insulating adhesive tape 108 comprising polyimide as a base and having a width of 10 mm, a length of 280 mm, and a thickness of 50  $\mu$ m was applied to one side of the front surface (upper electrode layer 105 side) of the photovoltaic element such that the tape 108 was opposed to the back-surface-side conductive foil 109.

Subsequently, a carbon-coating wire comprising a copper wire of 100  $\mu$ m diameter coated with carbon paste was formed on the front side surface of the photovoltaic element as a collecting electrode 106. In this case, the carbon-coating wires were continuously formed on the upper electrode layer 105 and the insulating adhesive tape 108 at a pitch of 14 mm in such a manner that the wires crossed the insulating tape.

Furthermore, a front-surface-side conductive foil 107 that was a further collecting electrode different from the collecting electrode 106 was formed on the insulating adhesive tape 108. The front-surface-side conductive foil 107 was formed by placing a copper foil strip of 20 mm in width, 285 mm in length, and 100  $\mu$ m in thickness on the insulating adhesive tape 108 with interposition of a part of the collecting electrode 106 therebetween, and heating, pressurizing, fixing the strip at 200°C and 3 kg/cm<sup>2</sup> for 180 seconds. One side of the copper foil strip is protruded out from the photovoltaic element 100 at a side opposite to the back-surface-side conductive foil 109, as shown in Fig. 1A.

To use for electric power generation the photovoltaic element produced in this manner, a plurality of photovoltaic elements were electrically connected in series to produce a photovoltaic element module. The connection method is described in Figs 2A to 2C.

As shown in Figs. 2A to 2C, two adjacent photovoltaic elements were arranged in such a way that a part of the front-surface-side conductive foil 107 of a photovoltaic element 1 overlapped a part of the back-surface-side conductive foil 109 of a photovoltaic element 2 over a distance of 3 mm.

Then, the overlapping portion between the front-

surface-side conductive foil 107 of the photovoltaic element 1 the back-surface-side conductive foil 109 of the photovoltaic element 2 was irradiated with laser light to be welded, thereby mechanically and electrically connect the two elements together.

Reference numeral 110 is a welding point. The laser for providing a high power enough to weld a metal preferably has a wavelength of  $0.4\text{ }\mu\text{m}$  and more and is particularly preferably a solid laser having a wavelength of  $0.4\text{ }\mu\text{m}$  to  $2.0\text{ }\mu\text{m}$ . The applicable laser includes a YAG laser, a phosphate glass laser, a silicate glass laser, and a  $\text{CO}_2$  laser. This example used a YAG laser (wavelength:  $1.06\text{ }\mu\text{m}$ ) was used to carry out welding under the following conditions: outgoing energy: 15.0J; pulse width: 5.0 ms; welding point diameter: 0.5 mm; number of welding points: 6.

Subsequently, the electric resistance of the laser welded portion was measured at  $0.013\text{ }\Omega$ . With respect to the performance of the photovoltaic element 100, the effective area was  $809.0\text{ cm}^2$ , the generated current density was 5.38 A, the generated current was 5.38 A, the generated voltage was 1.2 V, and the generated electric power was 6.45 W, therefore the resistance loss of the laser welded portion was 0.9 mW. This corresponds to only 0.015% of the electric power generated by the photovoltaic element 100.

In addition, the tensile strength of the laser

welded portion was measured to be in a range of 8 kg to 15 kg.

In this example, with respect to the time required for laser welding, 2.0 seconds were required for feed-in and positioning of the photovoltaic elements 1 and 2, 3.5 seconds were required for welding (including the movement of the laser beam outgoing tip), and 1.0 second was required for feed-out of the elements.

Thus, the connection of the two photovoltaic elements was completed in 6.5 seconds.

That is, this example can provide a reliable series-connected photovoltaic element module that is produced at a speed higher than that of the conventional examples, and a method of producing it. (Example 2)

Figs. 3A to 4C are schematic views showing the appearance of a photovoltaic element module according to Example 2 of the present invention. Fig. 3A is a plan view of a photovoltaic element as seen from its light-receiving surface, and Fig. 3B is a sectional view of the photovoltaic element shown in Fig. 3A, which is taken along the line 3B-3B in Fig. 3A. In addition, Fig. 4A is a plan view of two photovoltaic elements connected in series as seen from their light-receiving surface, Fig. 4B is an enlarged view of the series-connected portion in Fig. 4A, and Fig. 4C is a sectional view of Fig. 4B.

In this example, a material was previously plated with Ni on a portion to be irradiated with laser light. The Ni plating was used as a medium capable of absorbing light.

5 In Fig. 3A, reference numeral 200 indicates a 300 mm x 280 mm photovoltaic element comprising a substrate 202, a lower electrode layer 203, a semiconductor layer 204 consisting of amorphous silicon and having a photovoltaic function, and an upper electrode layer 10 205. Reference numeral 201 designates an etching line, 206 a collecting electrode, 207 a front-surface-side conductive foil that is a further collecting electrode different from the collecting electrode 206, 208 an insulating adhesive tape, and 209 a back-surface-side 15 conductive foil. These components were formed of the same materials as in Example 1 by using the same method as in Example 1. The front-surface-side conductive foil 207 and the rear-surface-side conductive foil 209 were formed so as not to protrude out from the 20 photovoltaic element 200.

A plurality of the above photovoltaic elements were electrically connected in series. The connection method is described with reference to Figs. 4A to 4C.

25 This example used a connection member 211 for connections. First, the metal member 211 which was the connection member was arranged in such a way as to contact the photovoltaic elements 1 and 2, as shown in

Fig. 4C. Then, the metal member was irradiated with YAG laser light (indicated by the arrows in Fig. 4C) in the same manner as in Example 1 except for the use of 6.0J outgoing energy. Reference numeral 210 denotes a welding point. The metal member 211 comprised an Ni-plated copper material (width: 10 mm; length: 275 mm; thickness: 100  $\mu$ m) consisting of an inexpensive and conductive copper material plated with an Ni material having a thickness of 2  $\mu$ m which absorbs about 50% of YAG laser light having a wavelength of 1.06  $\mu$ m. Since Ni absorbs YAG laser light much better than copper (that is, Ni has fewer losses caused by reflection from the surface of the metal), the outgoing energy of the YAG laser could be restrained. This example used 6.0J outgoing energy from the YAG laser, but good welding results could be obtained under this condition as in Example 1.

Although in this example the medium capable of absorbing light was provided by plating the metal material (copper material) with Ni, the effects shown in Fig. 15 as described above could be obtained when a metal member coated with carbon black was used.

That is, this example can provide a reliable series-connected photovoltaic element module that requires lower costs than Example 1 and that operates faster than the conventional examples, and its producing method.



(Example 3)

Figs. 5A and 5B and 6A to 6C are schematic views showing the appearance of a photovoltaic element module according to Example 3 of the present invention. Fig.

5 5A is a plan view of a photovoltaic element as seen from its light-receiving surface, and Fig. 5B is a sectional view of the photovoltaic element shown in Fig. 5A, which is taken along the line 5B-5B in Fig. 5A. In addition, Fig. 6A is a plan view of two  
10 photovoltaic elements connected in series as seen from their light-receiving surface, Fig. 6B is an enlarged view of the series-connected portion in Fig. 6A, and Fig. 6C is a sectional view of Fig. 6B.

In this example, a portion to be irradiated with  
15 laser light was previously coated with a color ink as a medium capable of absorbing light.

In Fig. 5A, reference numeral 300 indicates a 300 mm x 280 mm photovoltaic element comprising a substrate 302, a lower electrode layer 303, a semiconductor layer  
20 304 consisting of amorphous silicon and having a photovoltaic function, and an upper electrode layer 305. Reference numeral 301 designates an etching line, 306 a collecting electrode, 307 a front-surface-side conductive foil that is a further collecting electrode  
25 different from the collecting electrode 306, 308 an insulating adhesive tape, and 309 a back-surface-side conductive foil. These components were formed of the

same materials as in Example 1 by using the same method as in Example 1.

A plurality of the above photovoltaic elements were electrically connected in series. The connection method is described with reference to Figs. 6A to 6C.

As shown in Figs. 6A to 6C, two adjacent photovoltaic element were arranged in such a way that a part of the front-surface-side conductive foil 307 of the photovoltaic element 1 and a part of the back-surface-side conductive foil 309 of the photovoltaic element 2 overlapped each other over a distance of 3 mm.

Then, a blue felt pen (Oily Magic ink No. 500) was used to coat a color ink 313 (having an absorptivity of 30% at a wavelength of  $1.06 \mu\text{m}$ ) as a medium capable of absorbing light on the overlapping portion of the front-surface-side conductive foil 307 of the photovoltaic element 1. Welding points 310 in the area coated with the color ink 313 were irradiated with YAG laser under the same conditions as in Example 2 to mechanically and electrically connect the two conductive foils to each other. For example, a solid laser having a wavelength of  $0.4 \mu\text{m}$  to  $2.0 \mu\text{m}$  may be used instead of the YAG laser.

This example provided good results similar to Example 2.

Similar results were obtained by using a color ink

having an absorptivity of 10% (a sky blue felt pen) in place of the color ink 313 used in this example. In addition, similar results were obtained by using ink jet or silk screen printing instead of a felt pen.

5 (Example 4)

10 Figs. 7A and 7B and 8A to 8C are schematic views showing the appearance of a photovoltaic element module according to Example 4 of the present invention. Fig. 7A is a plan view of a photovoltaic element as seen from its light-receiving surface, and Fig. 7B is a sectional view of the photovoltaic element shown in Fig. 7A, which is taken along the line 7B-7B in Fig. 7A. In addition, Fig. 8A is a top view of two photovoltaic elements connected in parallel as seen from their light-receiving surface, Fig. 8B is an enlarged view of the series-connected portion in Fig. 8A, and Fig. 8C is a sectional view of Fig. 8B.

15 In this example, metal substrates were connected in parallel by using laser welding. In Fig. 7A, reference numeral 400 indicates a 300 mm x 280 mm photovoltaic element comprising a substrate 402, a lower electrode layer 403, a semiconductor layer 404 consisting of amorphous silicon and having a photovoltaic function, and an upper electrode layer 20 405. Reference numeral 401 designates an etching line, 406 a collecting electrode, 407 a front-surface-side conductive foil that is a further collecting electrode 25

different from the collecting electrode 406, 408 is an insulating adhesive tape. These components were formed of the same materials as in Example 1 by using the same method as in Example 1. Since, however, the metal  
5 substrate 402 was used as a back-surface-side terminal, the back-surface-side conductive foil was not particularly provided. In addition, the front-surface-side conductive foil 407 was formed so as not protrude out from the photovoltaic element 400.

10 A plurality of photovoltaic elements were electrically connected in parallel. The connection method is described with reference to Figs. 8A to 8C.

As shown in Figs. 8A to 8C, two adjacent  
15 photovoltaic element were arranged in such a way that the substrate 400 of the photovoltaic element 1 and the substrate 400 of the photovoltaic element 2 closely contact each other. The closely contacting portion between the two substrates was irradiated with YAG laser light to weld and connect them to each other.  
20 Although this example used the YAG laser, one of the other lasers described above may be used. Since this example used as the substrate 400 stainless steel mainly consisting of Fe (having an absorptivity of about 30% at a wavelength of 1.06  $\mu\text{m}$ ), stable welding  
25 could be achieved with a low energy.

Subsequently, a metal member 411 that was a connection member was arranged in such a way as to

contact the front-surface-side conductive foils 407 of the photovoltaic elements 1 and 2, and the metal member 411 was irradiated with YAG laser light to weld the elements together in order to connect them in parallel.

5 Reference numeral 410 indicates a welding point. The metal member 411 was similar to the metal member 211 and the welding conditions were similar to these in Example 2.

10 The present invention enables both the front and back sides to be stably welded with low costs and provides a parallel-connected photovoltaic element module having an excellent connection stability and a method of producing it.

(Example 5)

15 Figs. 9A to 10C are schematic views showing the appearance of a photovoltaic element module according to Example 5 of the present invention. Fig. 9A is a plan view of a photovoltaic element as seen from its light-receiving surface, and Fig. 9B is a sectional view of the photovoltaic element shown in Fig. 9A, which is taken along the line 9B-9B in Fig. 9A. In addition, Fig. 10A is a plan view of two photovoltaic elements connected in series as seen from their light-receiving surface, Fig. 10B is an enlarged view of the series-connected portion in Fig. 10A, and Fig. 10C is a sectional view of Fig. 10B.

25 In this example, a film was previously arranged on

a portion to be irradiated with laser light, as a medium capable of absorbing light.

In Fig. 9A, reference numeral 500 indicates a 300 mm x 280 mm photovoltaic element comprising a substrate 502, a lower electrode layer 503, a semiconductor layer 504 consisting of amorphous silicon and having a photovoltaic function, and an upper electrode layer 505. Reference numeral 501 designates an etching line, 506 a collecting electrode, 507 a front-surface-side conductive foil that is a further collecting electrode different from the collecting electrode 506, 508 an insulating adhesive tape, and 509 a back-surface-side conductive foil. These components were formed of the same materials as in Example 1 by using the same method as in Example 1. The back-surface-side conductive foil 509 was formed so as not to protrude out from the photovoltaic element 500. The front-surface-side foil 507 was 10 mm in width, 285 mm in length, and 100 $\mu$ m in thickness, and one side of the foil 507 extended outward from the photovoltaic element 500.

A plurality of photovoltaic elements were electrically connected in series. The connection method is described with reference to Figs. 10A to 10C.

As shown in Figs. 10A to 10C, two adjacent photovoltaic element were arranged in such a way that a part of the front-surface-side conductive foil 507 of the photovoltaic element 1 and a part of the back-

surface-side conductive foil 509 of the photovoltaic element 2 overlapped each other over a distance of 3 mm. In this case, the interval between the photovoltaic elements 1 and 2 was 2 mm.

5 A film 513 was arranged as a medium capable of absorbing light on the overlapping portion between the front-surface-side conductive foil 507 of the photovoltaic element 1 and the back-surface-side conductive foil 509 of the photovoltaic element 2,.

10 This example used a black PET (polyethylene-terephthalate) tape (Melinex 427, produced by ICI Japan Ltd.; absorptivity at a wavelength of  $1.06\text{ }\mu\text{m}$ : 65%; thickness  $20\text{ }\mu\text{m}$ ; width: 13 mm) was used as the film 513. Welding points (not shown in the drawings) on the  
15 surface of the film 513 were irradiated with YAG laser light as shown by the arrows in Fig. 10C to mechanically and electrically connect the two conductive foils to each other. For example, a solid  
20 laser having a wavelength of  $0.4\text{ }\mu\text{m}$  to  $2.0\text{ }\mu\text{m}$  may be used instead of the YAG laser.

This example provided good results similar to Example 2.

When a film is used as the medium as in this example, a film having a thickness of  $5\text{ }\mu\text{m}$  to  $30\text{ }\mu\text{m}$  is  
25 preferable because the film can be easily removed after welding. When the thickness of the film is smaller than  $5\text{ }\mu\text{m}$ , the film is likely to be torn off while

being peeled off. In addition, when the thickness of the film is larger than 30  $\mu\text{m}$ , the adhesion strength of the film becomes excessively high as shown in Fig. 16, thereby requiring a strong force for peeling the film

5 off. As a result, the welded metal member may be deformed or the film may be torn off. In Fig. 16, symbol (1) designates Lumirror X (produced by Toray Industries, Inc.), symbol (2) denotes Melinex 427 (produced by ICI Japan Ltd.), or symbol (3) indicates  
10 OPP silicon (produced by Panac Co., Ltd.). Fig. 16 shows the results obtained when used the films (1), (2) and (3). Such an increase in adhesion strength is caused by the adhesion of the film base material (medium) melted by laser light of a constant diameter  
15 to the metal member. This characteristic has no problem when the film base material is so thin that only a small amount of base material is melted, whereas when the thickness of the film base material is beyond a constant value, the melted amount of base material  
20 and the adhesion strength exhibit a positive correlation, thereby resulting in a problem.

The present invention is not limited to the above examples.

(Example 6)

25 According to this example, an aluminum sheet that constituted an electrode for an electric part was cut. Fig. 17 is a schematic view showing a laser treatment



method according to Example 6 of the present invention.

In Fig. 17, reference numeral 800 indicates the irradiation of CO<sub>2</sub> laser excited infrared light, and reference numeral 801 indicates a non-adhering medium consisting of black polyethyleneterephthalate film 10mm in thickness, 13 cm in length, and 0.3 mm in thickness. Although this example used as the non-adhering medium 801 a Melinex 427 film produced by ICI Japan Ltd., the experiments conducted by the inventors confirmed that performance similar to that of this example could be obtained when used Lumirror X30 produced by Toray Industries, Inc. The surface roughness of the non-adhering medium 801 was measured to be in a range of 0.1 nm to 2 nm in mean square, by using a three-dimensional surface roughness meter of non-contact optical system. In addition, reference numeral 802 indicates a material to be treated consisting of an aluminum sheet having a length of 10 cm and a thickness of 0.5 mm.

The material 802 to be treated was fixed to a jig (not shown in the drawings) having a groove formed at a laser irradiation position, and a non-adhering medium 801 was placed on the material 802 to be treated at a position to be irradiated with laser light.

Subsequently, a presser jig (not shown in the drawings) having at a cutting position a groove to be penetrated by laser light was used to closely contact the non-

adhering medium 801 with the material 802 to be treated under 1 kg/cm<sup>2</sup> pressure. Subsequently, using Ar as a shield gas, the material to be treated was irradiated with laser light 800 along the groove to be penetrated by the light to cut the material 802. The irradiation conditions of the laser light 800 were as follows: outgoing energy: 25J; pulse width: 3 ms; pulse repetition speed: 15 PPS; laser beam diameter:  $\phi 0.5$  mm.

The laser irradiated portion of the non-adhering medium 801 was melted and evaporated by the irradiation of laser light. Once cutting was completed by using laser light, the presser jig was opened and the remaining non-adhering medium 801 was removed by using tweezers to complete the series of operations. Although this example used the tweezers to remove the non-adhering medium 801, a method of blowing the medium off by using a shield gas may be suitably used.

Since in this example the non-adhering medium 801 was placed on the laser light-irradiated surface of the material to be treated, the amount of energy required for cutting could be remarkably reduced. Furthermore, since the non-adhering medium 801 is removed after laser irradiation, no non-adhering medium 801 remains after the series of operations have been finished, thereby avoiding appearance problems and preventing problems from occurring in the post-process.

This example provides stable laser treatment

because, in this example, laser treatment can be carried out with a lower energy than that of the conventional techniques and the reflectance is determined depending on the physical characteristics of the placed non-adhering medium. In addition, the material is treated while holding the non-adhering medium, thereby enabling stable close contact and thus stable laser treatment. Furthermore, the operator must only place the non-adhering medium, thereby increasing the treatment speed. In addition, since the non-adhering medium can be easily removed after laser treatment, the present example provides a laser treatment method that avoids appearance problems while preventing problems from occurring in the post-process.

(Example 7)

This example used laser light to weld the electrodes of photovoltaic elements, the electrodes consisting of a copper foil.

Figs. 18A and 18B and 19A to 19C are schematic views showing the appearance of a photovoltaic element module according to Example 7 of the present invention. Fig. 18A is a plan view of a photovoltaic element as seen from its light-receiving surface, and Fig. 18B is a sectional view of the photovoltaic element shown in Fig. 18A, which is taken along the line 18B-18B in Fig. 18A. In addition, Fig. 19A is a plan view of two photovoltaic elements connected in series as seen from

their light-receiving surface, Fig. 19B is an enlarged view of the series-connected portion in Fig. 19A, and Fig. 19C is a sectional view of Fig. 19B. Fig. 20 is a schematic view showing the method of supplying non-adhering and anti-reflection materials according to Example 7.

In Fig. 18A, reference numeral 900 indicates a 300 mm x 280 mm photovoltaic element comprising a substrate 902, a lower electrode layer 903, a semiconductor layer 904 consisting of amorphous silicon and having a photovoltaic function, and an upper electrode layer 905.

In this example, the substrate for supporting the entire photovoltaic element comprises a stainless steel plate having a thickness of 150  $\mu\text{m}$ . An Al layer of about 2,000  $\text{\AA}$  in thickness and a ZnO layer of about 13,000  $\text{\AA}$  in thickness were sequentially formed on the substrate 902 as the lower electrode layer 903 by using the sputtering method. In addition, the semiconductor layer 904 was formed by sequentially stacking an n-, i-, p-, n-, i-, and p-type semiconductor layers in this order from the substrate side by using the plasma CVD method. The thicknesses of these layers were about 150  $\text{\AA}$ , 4,000  $\text{\AA}$ , 100  $\text{\AA}$ , 100  $\text{\AA}$ , 800  $\text{\AA}$ , and 100  $\text{\AA}$ , respectively. In addition, the upper electrode layer 905 was a transparent electrode consisting of a thin indium oxide film of about 700  $\text{\AA}$  in thickness, and was

formed by depositing In in an O<sub>2</sub> atmosphere by using the resistance heating method. Furthermore, to prevent an effective light-receiving area from being affected by the adverse effect of a short circuit between the substrate and the transparent electrode that may occur when the outer circumference of the photovoltaic element is cut, etching paste containing FeCl<sub>3</sub> or AlCl<sub>3</sub> was coated on a part of the upper electrode layer 905 by using screen printing, and was heated and washed to linearly remove the part of the upper electrode layer 905 to thereby form an etching line 901.

Subsequently, a copper foil strip having a width of 10 mm, a length of 285 mm, and a thickness of 100 μm was formed near one side (280 mm long) of the back surface (on the substrate 902 side) of the photovoltaic element as a back-surface-side conductive foil 909, by using the method disclosed in Japanese Patent Application Laid Open No. 8-139349. One side of the copper foil strip protruded out from the photovoltaic element, as shown in Fig. 18A.

Subsequently, an insulating adhesive tape 908 comprising polyimide as a base and having a width of 10 mm, a length of 280 mm, and a thickness of 50 μm was applied to one side of the front surface (on the upper electrode layer 905) of the photovoltaic element such that the tape 908 is opposed to the back-surface-side conductive foil 909.

Subsequently, a carbon-coating wire comprising a copper wire of 100  $\mu\text{m}$  in diameter coated with carbon paste was formed on the front surface of the photovoltaic element as a collecting electrode 906. In this case, the carbon-coating wires were continuously formed on the upper electrode layer 905 and the insulating adhesive tape 908 at a pitch of 14 mm such that the wires crossed the insulating tape.

Furthermore, a front-surface-side conductive foil 907 that was a further collecting electrode different from the collecting electrode 906 was formed on the insulating adhesive tape 908. The front-surface-side conductive foil 907 was formed by placing a copper foil strip having a width of 10 mm, a length of 285 mm, and a thickness of 100  $\mu\text{m}$  on the insulating adhesive tape 908 with interposition of a part of the collecting electrode 906 therebetween and heating, pressurizing, fixing the strip at 200°C and 1 kg/cm<sup>2</sup> for 60 seconds. One side of the copper foil strip was protruded out from the photovoltaic element 900 on a side opposite to the back-surface-side conductive foil 909, as shown in Fig. 18A.

To use for electric power generation the photovoltaic element produced in this manner, a plurality of photovoltaic elements were electrically connected in series to produce a photovoltaic element module. The connection method is described in Figs.

19A to 19C.

As shown in Figs. 19A to 19C, two adjacent photovoltaic elements were arranged such that a part of the front-surface-side conductive foil 907 of a photovoltaic element 1 overlapped a part of the back-surface-side conductive foil 909 of a photovoltaic element 2 over a distance of 3 mm.

Subsequently, a non-adhering medium 913 was placed on the overlapping laser-welded portion between a part of the front-surface-side conductive foil 907 of the photovoltaic element 1 and a part of the back-surface-side conductive foil 909 of the photovoltaic element 2. As the non-adhering medium 913, a commercially available magnetic tape was used which comprises a magnetic substance such as carbon black coated or deposited on one side of polyethyleneterephthalate or polyethylenenaphthalate. This example used T-120VF produced by Sony Corporation, but the experiments conducted by the inventors confirmed that performance similar to that of this example can be obtained when used other magnetic tapes such as P6-120HMP2 or VXST-120VF produced by Sony Corporation or NV-ST120XPZ or NV-TTC40HGK produced by Matsushita Electric Industrial Co., Ltd., or heat transfer ribbons such as TL-12K produced by King Jim Co., Ltd., CF-PR190 produced by Matsushita Electric Industrial Co., Ltd., or JW-Z180 produced by Toshiba Corporation. Since these magnetic

tapes are supplied from the form of a roll, the subsequent laser treatment can be prepared by, after laser treatment, releasing the presser jig and feeding the tape forward. In addition, the surface roughness of the magnetic surfaces of these magnetic tapes was measured to be in a range of 5 nm to 20 nm in mean square.

Furthermore, a presser jig (not shown in the drawings) was used to press the magnetic tape which was the non-adhering medium 913 at 10 kg/cm<sup>2</sup> with the magnetic surface facing the front-surface-side conductive foil 907 of the photovoltaic element 1 which was a material to be treated.

Then, the overlapping portion between the front-surface-side conductive foil 907 of the photovoltaic element 1 and the back-surface-side conductive foil 909 of the photovoltaic element 2 which was pressed by the presser jig, was irradiated with laser light to carry out welding and mechanically and electrically connect the elements to each other. Reference numeral 910 designates a welding point. As the laser for providing a high energy enough to weld a metal, it is possible to use a YAG laser, a phosphate glass laser, a silicate glass laser, or a CO<sub>2</sub>-laser-excited far infrared laser. In particular, the YAG laser has excellent characteristics such as its capability of transmitting laser light through optical fibers to enable treatment



at a position remote from the laser oscillator, and enables the welding condition to be changed by the selection of the optical fibers and an outgoing unit. Another excellent characteristic of this laser is its capability of dividing a laser light into 2 to about 10 beams.

This example used the YAG laser to execute welding under the following conditions: outgoing energy: 6J; pulse width: 5 ms: laser diameter: 0.6 mm; number of welding points: 12.

The method of supplying the magnetic tape as the non-adhering medium 913 according to this example is described with reference to Fig. 20. In this figure, reference numeral 920 indicates a magnetic tape housed in a cassette, 921 a reel around which a magnetic tape irradiated with laser light is wound, and 922 a presser member for pressing the magnetic tape 913 against a junction portion between the front-surface-side conductive foil 907 of the photovoltaic element 1 and the back-surface-side conductive foil 909 of the photovoltaic element 2 which are materials to be treated. A transfer means (not shown in the drawings) is used to transfer to a laser treatment position the front-surface-side and back-surface-side conductive foils 907 and 909 of the photovoltaic elements 1 and 2, respectively. Then, the presser jig 922 presses the magnetic tape 913 against the junction portion between

the front-surface-side conductive foil 907 of the photovoltaic element 1 and the back-surface-side conductive foil 909 of the photovoltaic element 2. Subsequently, the junction portion is irradiated with laser light 930 to carry out a predetermined laser treatment.

The portion of the magnetic tape 913 irradiated with laser light is melted and evaporated by the heat generated by welding. Furthermore, since a magnetic substance having a surface roughness of 5 nm to 20 nm in mean square is coated or deposited on the surface of the magnetic tape 913 closely contacting the front-surface-side conductive foil 907 of the photovoltaic element 1, after welding, the magnetic tape 913 can be removed by simply releasing the presser jig. The magnetic tape 913 may adhere to the front-surface-side conductive foil 907 in some cases, the tape can be easily removed by applying a force enough to slightly release the tape from the foil (not shown in the drawings).

Subsequently, the magnetic tape 913 is fed by 3 cm so as to be wound around the winding reel 921, and an unused magnetic tape is supplied from the magnetic tape cassette 920 to complete preparations for the subsequent laser treatment. The treated photovoltaic elements 1 and 2 are conveyed out by a transfer means (not shown in the drawings) immediately after laser

treatment.

The electric resistance of the laser welded portion was measured to be  $0.013 \Omega$ . With respect to the performance of the photovoltaic element 900, the effective area was  $809.0 \text{ cm}^2$ , the generated current was 5.38 A, the generated voltage was 1.2 V, and the generated power was 6.45 W, therefore the resistance loss of the laser welded portion was 0.9 mW, which is only 0.015% of the generated electric power of 6.45 W.

In addition, the tensile strength of the laser welded portion was measured to be in a range of 8 kg to 15 kg.

In this example, with respect to the time required for laser welding, 2.0 seconds were required to feed-in and positioning of the photovoltaic elements 1 and 2, 3.5 seconds were required for welding (including the movement of the laser beam outgoing tip), and 1.0 second was required for feed-out of the treated elements. Thus, the connection of the two photovoltaic elements was completed in 6.5 seconds.

That is, this example can provide a method of connecting photovoltaic elements in series that enables laser welding with a lower energy than that of the conventional techniques, that enables high speed treatment, and that avoids appearance problems while preventing problems occurring in the post-process.

The present invention minimizes the time required

for heating when executed to connect a group of photovoltaic elements, thereby preventing the components of the photovoltaic elements such as the semiconductor layer and conductive adhesive from being degraded by wide-ranging heating.

In addition, in the present invention, each operation can be completed in a short time to enable mass production.

Furthermore, the present invention eliminates the needs for solder to avoid reduction of the production yield due to solder residues and avoid the adverse effect of remaining fluxes on a covering material.

In addition, the present invention uses the color ink or film to easily increase the laser absorption efficiency, thereby providing an inexpensive photovoltaic element production method having a high production efficiency.

Furthermore, in the method of placing the non-adhering medium on the surface to be irradiated with laser light of the material to be treated, and irradiating the non-adhering medium with laser light while holding the non-adhering medium and the material, laser treatment can be stably executed because the reflectance is determined depending on the physical properties of the placed material (non-adhering medium). In addition, the treatment can be carried out while holding the non-adhering medium and the material

to be treated, thereby enabling stable close contact therebetween and thus stable laser treatment.

Moreover, high speed treatment is possible because of only placing the non-adhering medium.

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